TDA Progress Report 42-95

July-September 1988

## Deriving a Geocentric Reference Frame for Satellite Positioning and Navigation

R. P. Malla<sup>†</sup> S.-C. Wu

Tracking Systems and Application Section

With the advent of Earth-orbiting goedetic satellites, nongeocentric datums or reference frames have become things of the past. Accurate geocentric three-dimensional positioning is now possible and is of great importance for various geodetic and oceanographic applications. While relative positioning accuracy of a few centimeters has become a reality using very-long-baseline interferometry (VLBI), the uncertainty in the offset of the adopted coordinate system origin from the geocenter is still believed to be on the order of 1 meter. Satellite laser ranging (SLR), however, is capable of determining this offset to better than 10 cm, but this is possible only after years of measurements. Global Positioning System (GPS) measurements provide a powerful tool for an accurate determination of this origin offset. Two strategies are discussed in this article. The first strategy utilizes the precise relative positions that have been predetermined by VLBI to fix the frame orientation and the absolute scaling, while the offset from the geocenter is determined from GPS measurements. Three different cases are presented under this strategy. The reference frame thus adopted will be consistent with the VLBI coordinate system. The second strategy establishes a reference frame by holding only the longitude of one of the tracking sites fixed. The absolute scaling is determined by the adopted gravitational constant (GM) of Earth; and the latitude is inferred from the time signature of Earth rotation in the GPS measurements. The coordinate system thus defined will be a geocentric Earth-fixed coordinate system. A covariance analysis shows that geocentric positioning to an accuracy of a few centimeters can be achieved with just one day of precise GPS pseudorange and carrier phase data.

#### I. Introduction

The fully operational Global Positioning System (GPS) will consist of at least 18 satellites distributed in six orbital planes [1]. This system will allow a user, anywhere on the Earth or in a low Earth orbit, to view at least five satellites most of the

†Member of Professional Staff, Sterling Software, Pasadena, CA.

time. Two precision data types can be derived from the GPS transmitted signals: P-code pseudorange and carrier phase at two L-band frequencies [2]. These precision data types provide the opportunity to produce geodetic measurements accurate to the centimeter level [3] and orbit determination of low Earth orbiters to the subdecimeter level [4]. The ephemerides for the GPS satellites, as distributed by Naval Surface Weapon Center (NSWC), are based upon the World Geodetic System

(WGS 84) [5], and their accuracy is on the order of 10 meters [6]. In applications where high precision is essential, the GPS satellite orbits need to be adjusted to a much higher precision, along with all the other parameters in the network [3], [4]. The GPS satellites can be simultaneously observed from several sites in a geodetic network. Within such a network a few fiducial tracking sites are included [7]. The relative positions of these fiducial sites are known to a higher level of precision. typically a few centimeters, as a result of repeated measurements of the baselines using very-long-baseline interferometry (VLBI) [8]. Based upon these highly precise relative positions of the fiducial sites, filter strategies can be designed to adjust the satellite orbits to enhance their accuracy to far better than 10 meters [9]. The ephemerides thus adjusted now refer to the same coordinate frame in which the fiducial baselines are known. It is generally believed that the best VLBI coordinate system origin approximates the geocenter to about 1 meter. The satellite laser ranging (SLR) technique is capable of realizing the geocenter offset to better than 10 cm, but this is possible only after years of observations.

Although absolute positioning is of less interest for geodynamic applications, it can be an important factor when tracking deep space vehicles, and it is essential for orbit determination of Earth-observing satellites, such as NASA's Ocean Topography Experiment (TOPEX), to be launched in late 1991 [10]. This article investigates two strategies for precise determination of the geocenter, thus establishing a geocentric coordinate frame for GPS measurements. In the first strategy, GPS P-code pseudorange and carrier phase measurements are made from a set of globally distributed tracking stations. A network consisting of six stations appears to be appropriate. Of these, three are the fiducial sites whose relative location has been well determined by VLBI. Since it is the relative location, rather than the absolute location, of the fiducial sites that is well determined by VLBI, only baseline coordinates should be fixed to define the orientation and absolute scaling of the reference frame. The geocenter position and the coordinates of other, nonfiducial sites are to be adjusted together with the GPS orbits. The coordinate frame thus defined is consistent with the VLBI frame, with improved geocenter offset. Three different cases are discussed under this strategy.

An alternate strategy is to simultaneously adjust the GPS orbits and geodetic station coordinates with respect to one reference site in the network whose longitude is held fixed. The absolute scaling is determined by the adopted gravitational constant GM of Earth; the station heights are inferred from the adjusted periods of GPS orbits and the pseudorange measurements; and the latitude is inferred from the time signature of Earth rotation in the GPS measurements. The coordinate system thus defined will be an Earth-centered,

Earth-fixed (ECEF) coordinate frame. The solution is free from any a priori uncertainty of site positions, and the inferred reference frame is strictly self-contained. This type of technique has been adopted by the satellite laser ranging (SLR) and lunar laser ranging (LLR) communities [11]. The coordinate origin offset from the geocenter is given by the weighted mean coordinate offsets of all stations in the network.

A covariance analysis was performed estimating the accuracy with which the geocenter position can be determined using the two strategies. This analysis indicates that the geocenter position can be determined to an accuracy of a few centimeters with just one day of precision pseudorange and carrier phase data. Such precise knowledge of absolute position of the coordinate system origin is essential to the orbit determination of TOPEX, which requires an altitude accuracy of 13 cm or better.

#### II. Coordinate Reference Frame

A rectangular coordinate system is defined such that the Z axis coincides with the mean spin axis of the Earth as defined by the CIO pole; the X axis lies in the mean equatorial plane, which is perpendicular to the Z axis, and passes through the mean Greenwich astronomic meridian as defined by the BIH; the Y axis completes the right-handed Earth-fixed cartesian system. The origin of the coordinate system may be defined as the center of mass of the Earth. But the imperfect knowledge of the geocenter location limits the precise location of this origin.

Figure 1 gives the definition of the World Geodetic System 84 (WGS 84). The almanac and the ephemerides of GPS satellites are given in this coordinate system [6]. The coordinates of the ground stations derived by observing the GPS measurements will also be in the WGS 84 reference frame. But it should be noted that the absolute accuracy of any geocentric position determination depends upon the knowledge of the location of the geocenter relative to the assumed origin. The coordinate system thus defined is an ECEF coordinate system which rotates at a constant mean rate around a mean astronomic pole. Such a system is also called a conventional terrestrial system (CTS). However, events occur in an instantaneous real world, which is in a coordinate system different from the CTS. Therefore it is required to mathematically relate CTS to an instantaneous terrestrial system (ITS). This relationship is a transformation through a wobble [W] and a spin [S]:

$$\mathbf{X}_{\text{ITS}} = [S] [W] \mathbf{X}_{\text{CTS}} \tag{1}$$

where the X's are position vectors. The wobble [W] is given by

$$[W] = \mathbf{R}_{x}(-y_{n}) \mathbf{R}_{y}(x_{n}) \tag{2}$$

where  $\mathbf{R}_r(p)$  denotes a matrix of rotation, by an amount p about the r axis;  $x_p$  and  $y_p$  define the pole motion. The sign convention used is in accordance with the BIH convention. The spin is given by

$$[S] = R_z(-GAST)$$
 (3)

where GAST is the Greenwich Apparent Sidereal Time given by

GAST = GMST<sup>0h UT</sup> + 
$$\overline{\omega}$$
 ( $t_{df}$  + UT1 - UTC)  
+  $\Delta\Psi\cos\epsilon$  (4)

GMST<sup>0h</sup> UT is the Greenwich Mean Sidereal Time at 0 hour UT, which is obtained from Newcomb's equation adjusted with respect to J2000 [12],  $\overline{\omega}$  is the mean rate of advance of the GMST per day, and  $t_{af}$  is the day fraction in UTC of time of observation. The last term in Eq. (4) is commonly known as the equation of the equinoxes, where  $\Delta\Psi$  refers to the nutation in longitude and  $\epsilon$  is the true obliquity of the ecliptic of date.

In general, celestial bodies are expressed in the Conventional Inertial System (CIS). Position vectors in this system can be transformed into ITS through a nutation [N] and a precession [P] [13]:

$$\mathbf{X}_{CIS} = [\mathbf{P}] [\mathbf{N}] \mathbf{X}_{ITS} \tag{5}$$

The nutation [N] is given by

$$[\mathbf{N}] = \mathbf{R}_{\mathbf{x}}(-\epsilon_{\alpha}) \mathbf{R}_{\mathbf{x}}(-\Delta \Psi) \mathbf{R}_{\mathbf{x}}(\epsilon_{\alpha} + \Delta \epsilon)$$
 (6)

where  $\epsilon_0$  is the mean obliquity of date; the nutation angles  $\Delta\Psi$  and  $\Delta\epsilon$  are computed from IAU 1980 nutation series [12] expressed with respect to J2000. The precession [P] is given by

$$[\mathbf{P}] = \mathbf{R}_z(-\zeta_a) \, \mathbf{R}_v(-\theta_a) \, \mathbf{R}_z(z_a) \tag{7}$$

where  $\xi_a$ ,  $\theta_a$ , and  $z_a$  are the standard precession rotation angles [14]. Therefore, the position vectors in the reference frame WGS 84, which is one of the CTS, can be expressed with respect to the CIS using the above transformations.

The SLR system has matured enough to establish its own independent coordinate system. The dynamic technique used to establish such a system depends heavily upon a precise definition of the coordinate frame adopted by the tracking network. This includes the definition of polar motion and the Earth's fundamental constants, such as the gravitational constant (GM), the dynamical form factor (J<sub>2</sub>), and the speed of light. Because satellite (LAGEOS, STARLETTE, etc.) position

vectors are described in an inertial frame while ground station vectors are described in an ECEF frame, they need to be related by the above coordinate transformations. Processing of SLR long-arc data has been successful in simultaneously solving for station vectors, satellite orbits, and earth orientation parameters to precisions of few centimeters.

# III. Strategies to Determine the Origin Offset from the Geocenter

For the past several years the fundamental concept behind accurate GPS orbital adjustment has been that of the fiducial network [7]. A fiducial network consists of three or more tracking stations whose (relative) positions have been determined in an Earth-fixed coordinate frame to a very high accuracy, usually by VLBI. Several receivers at other, less accurately known, stations also observe simultaneously the GPS satellites along with the fiducial network. The data are then brought together to simultaneously adjust the GPS satellite orbits and the positions of the nonfiducial sites. Thus the fiducial stations established by VLBI provide a self-consistent Earth-fixed coordinate system with respect to which the improved GPS satellite orbits and the nonfiducial stations can be expressed to a greater accuracy. At the same time the coordinate frame origin offset from the geocenter can also be estimated using the same set of data. Experience in this area has indicated that an over-constrained network, where more baselines or sites than necessary are fixed, can in fact produce a degraded solution. This is because in an over-constrained network the a priori uncertainty in the fixed parameters that are more than necessary will result in a suboptimal filter weighting. The solution will then be highly influenced by the mismodeling of these parameters.

In the first strategy proposed, the fiducial baselines are treated in three different ways:

- (A) Fix two fiducial baselines.
- (B) Constrain two fiducial baselines by a priori weighting.
- (C) Fix only one fiducial baseline.

The baselines define the orientation of the adopted coordinate frame. The absolute scaling can be fixed either by the length of these baselines or by the Earth's gravitational constant, GM. Both are known to an accuracy of about one part in 10<sup>8</sup>. The baseline length is used to define the absolute scaling so that the resulting coordinate frame will be consistent with the VLBI frame defined by the fiducial baselines. For the case with two baselines fixed, it is rather convenient to select one of the fiducial stations common to both fixed baselines as the reference site. The filter process is so designed that the baselines between the reference site and all other

nonfiducial sites are adjusted along with the Earth Orientation Parameters (EOP), namely polar motion  $(x_p, y_p)$  and UT1-UTC rate, the GPS satellite orbits, and the absolute coordinates of the reference site, which in turn infer the adjustment of the geocenter position coordinates. The Earth's GM is also adjusted, although the data strength may not be great enough to improve the value of GM appreciably.

In the second strategy, the same GPS tracking network of globally distributed stations is used. However, only the longitude of a reference site is held fixed; all other site coordinates are adjusted simultaneously with the GPS orbits. Here, the GM of Earth provides the absolute scaling. The station heights can be derived from the adjusted periods of GPS orbits and pseudorange measurements. The time signature of the measurements defines the latitude. Figure 2 graphically demonstrates the time signature of the measurements for two hypothetical cases. The first graph shows the periodic signature generated by the pseudorange  $(\rho)$  measurements to an orbiting GPS from a stationary receiver. The period is equal to the GPS orbit period, which is nearly 12 hours, and the amplitude is proportional to the geocentric position vector of the receiver projected onto the orbital plane. The second graph shows the case when a stationary GPS satellite is above the equator of a spinning Earth. The period is now 24 hours, and the amplitude is proportional to the cosine of the receiver latitude. The variation of the signature with respect to the receiver latitude is depicted in the sketch. Because of the difference in period, the effects due to the rotation of the receiver can be separated from the GPS orbiting signature and the latitude can unambiguously be solved.

A simple mathematical model can be written out for the estimate of geocenter offset. This offset is expressed as the weighted mean of the position offsets of all stations. The equations corresponding to the geocenter offset  $\Delta G$  are represented as

$$\Delta G_x + \Delta x_i + \nu_i = 0, \qquad x \to y, z; \qquad (8)$$

$$i = 1, 2, \dots, n$$

where  $\Delta x_i$  is the x component of the  $i^{\text{th}}$  geocentric station position offset and  $\nu_i$  is the error associated with  $\Delta x_i$ . The corresponding error covariance of the geocenter offset can be expressed as

$$\operatorname{Var}(\Delta G) = [\mathbf{A}^{\mathrm{T}} \mathbf{W} \mathbf{A}]^{-1}$$

$$3 \times 3$$
(9)

where

$$\mathbf{A}^{\mathsf{T}} = [-\mathsf{I} - \mathsf{I} \dots - \mathsf{I}]$$

$$3 \times 3n$$

and W is a  $(3n \times 3n)$  weight matrix which is the inverted covariance matrix of the station position estimates.

### IV. Covariance Analysis

A covariance analysis was carried out to assess the accuracy with which the geocenter offset from the origin of the adopted coordinate frame can be determined with each of the approaches proposed in previous sections. A full constellation of 18 GPS satellites distributed in six orbital planes was assumed. A data arc spanning over 34 hours from a network of six globally distributed tracking stations was also assumed. The three fiducial sites are the three NASA Deep Space Network (DSN) tracking sites (Fig. 3) at Goldstone, California; Canberra, Australia; and Madrid, Spain. The remaining sites in Japan, Brazil, and South Africa are nonfiducial sites. Simultaneous GPS P-code pseudorange and carrier phase measurements are made at all of these stations. The relative positions of the three DSN sites have been measured repeatedly by VLBI over many years and are known to an accuracy of about 3 cm. Goldstone was selected to be the reference site because of its common VLBI visibility with the other two DSN sites at Canberra and Madrid. P-code pseudorange and carrier phase data noise were assumed to be 5 cm and 0.5 cm, respectively, when integrated over 30 minutes and corrected for ionospheric effects by dualfrequency combination.

Carrier phase biases were adjusted with a large a priori uncertainty. Table 1 lists the error sources assumed for the first strategy. The robustness of the GPS measurements allows all the GPS and station clocks to be treated as white-noise processes and adjusted [3], [4] to remove their effects on the solutions. Also adjusted are the zenith tropospheric delays at all ground sites, which were treated as random-walk parameters to model the temporal change. Such models have been proved to be effective in removing their errors without seriously depleting the data strength [9].

The GPS covariance and simulation analysis software system, OASIS [15], recently developed at JPL, was used to carry out the study. In OASIS, partial derivatives with respect to cartesian components of site locations and the geocenter are readily produced. It is shown in the Appendix that baseline partials are related to site location partials as follows.

(1) The partial derivative with respect to a cartesian component of the reference site is the sum of all partial derivatives with respect to the same component of all sites forming the baselines. Note that this is also the partial derivative with respect to the same component of the geocenter position.

(2) The partial derivative with respect to a baseline cartesian component is the same as the partial derivative with respect to the same component of the nonreference site forming the baseline.

Hence, the site location coordinate partials can readily be used in place of the baseline coordinate partials, and the geocenter offset coordinate partials in place of the reference site absolute coordinate partials.

The second strategy assumes the same network of six tracking sites. The estimated quantities are the coordinates of all six sites except the longitude of the reference site (Goldstone), together with the GPS satellite states, white-noise clocks, random-walk troposphere parameters, and carrier phase biases. Because the longitude of Goldstone is held fixed, the position components need to be given in a geodetic coordinate system, viz., longitude, latitude, and height. Table 2 lists the assumption variations that apply to this strategy. Other assumptions are kept the same as in Table 1. With this strategy, the error covariance matrix of geocenter offset is given by Eq. (9) in the previous section.

## V. Results of Covariance Analysis

In the covariance analyses for both strategies, data arcs of various lengths were used to study the solution convergence. In all cases the station at Goldstone was considered to be the reference site, although in the second strategy any of the ground sites can be a reference site where the only fixed component is the longitude.

Table 3 indicates the a priori error associated with the fiducial baselines, Goldstone-Canberra and Goldstone-Madrid, in all three cases of Strategy 1. The value of GM was adjusted, although it was found that the data strength of the GPS measurements is not great enough to improve on its a priori value. It should be noted that adjusting Earth's GM makes GPS satellite states consistent with the absolute scaling as implied by the baselines.

Figure 4 shows the total error of the origin offset as the length of the data span increases from 6 hours to 34 hours for Case A. At the end of 34 hours the origin offset error is 4.0 cm (rms of all three components). The bar chart shows a rapid reduction of error in origin offset between 6 and 12 hours. The result continues to improve after 12 hours but not at a very high rate. The reason for this can be seen in Fig. 5. After 12 hours the origin offset error has come down to the level of baseline error; data gathered thereafter only gradually reduces the effects of data noise. At the end of 34 hours the effect of data noise is reduced to 3.4 cm and would continue to reduce as the arc length increases. The contribution of the baseline

error, however, dropped to about 2.5 cm after 12 hours and remained virtually unchanged thereafter. This indicates that the geocenter can be determined only up to the a priori accuracy of the fiducial baselines. Therefore, with this strategy, any improvement on the baseline accuracy can improve the accuracy of the origin offset from the geocenter. For instance, it is customary to find baselines reported with a higher accuracy in length than in the other two components. When a smaller error of 1 cm is assumed for the fiducial baseline length, along with 3 cm for the transverse and vertical components, the rms error on the origin offset from the geocenter reduces to 3.5 cm with a 34-hour arc of GPS measurements. Figure 6 shows the origin offset error for Case B, where the baseline vectors constrained to their a priori error are also estimated. The geocenter offset error after 34 hours reduces to 3.8 cm. Note that the error involved here is mainly due to data noise alone. Results from Case C, where the Goldstone-Madrid baseline is the only baseline fixed, are plotted in Figs. 7 and 8. The geocenter offset error after 34 hours is 4.4 cm, which is slightly worse than the previous cases. In Fig. 8, however, the effect due to the fixed baseline reduces to 2 cm after 12 hours and settles at 1.7 cm after 18 hours. The effect due to the data noise will continue to decrease for longer data arc, but the baseline effect will remain unchanged, as shown by Figs. 5 and 8. When the EOP are not estimated, the geocenter offset error after 34 hours is found to be 4.1 cm. This slight improvement is due to reduced data noise effect when fewer parameters are estimated.

In the second strategy no tracking site coordinates, except the longitude of the site at Goldstone, were held fixed. Here, as before, simultaneous adjustment of all GPS satellite states, tracking site coordinates, carrier phase biases, and zenith tropospheric corrections were carried out for various arc lengths ranging between 6 and 34 hours. Figure 9 plots the variation of the rms error of the origin offset from the geocenter with respect to the data arc length. The errors affecting the origin offset from the geocenter in this strategy are the data noise and the GM of Earth, which defines the absolute scaling. At the end of 6 hours the rms error of the origin offset is 143.7 cm, which reduces to 8 cm at the end of 12 hours. This indicates that the control on the absolute scaling and the orientation in latitude is greatly improved after all the GPS satellites have been tracked by the globally distributed sites for a complete orbit cycle. At the end of 34 hours the rms error reduces to 2.1 cm. The graph shows a strong trend of decreasing rms error as the arc length increases. This indicates that the origin offset determination is limited only by the data noise. This result can be compared with Case C of Strategy 1 when EOP are not estimated; there is about a 50% improvement in the geocenter offset error with this method. The Earth's GM is known accurately enough so that its effect is on the order of 0.2 cm after 12 hours and is 0.1 cm at the end of 34 hours.

In the analysis of Strategy 2, the effects of polar motion and UT1-UTC have not been included. However, GPS measurements are insensitive to any constant UT1-UTC bias error. The analyses done with different cases of Strategy 1 have indicated that a constant bias for polar motion and a UT1-UTC rate can be included in the filter as additional adjusted parameters without significantly degrading the performance.

## VI. Effect of Coordinate Frame Origin Offset on Orbit Determination of Low Earth-Orbiting Satellite

To gain further insight into the significance of accurate definition of geocenter, the effect on the radial position of a low Earth-orbiting satellite, in particular TOPEX, was studied. The error assumptions used are the same as given in Table 1 except for those parameters listed in Table 4. The result presented by Case C of Strategy 1 shows that the origin offset accuracy is 4.4 cm (Fig. 7) with only one baseline fixed and a data arc of 34 hours. This value is the most pessimistic of all the results presented. Here, the origin offset was assumed to have an error of 4 cm in each component and left unadjusted. A reduced dynamic tracking technique [16] was implemented in the study where a fictitious 3-D force on TOPEX was adjusted as process noise with constrained a priori uncertainty. Figure 10 plots the error in the radial component of TOPEX caused by various sources. The total error in TOPEX altitude over the 2-hour arc has an rms value of 9.7 cm. Figure 11 shows the altitude error variation with time, along with the part contributed by a 4-cm geocenter uncertainty, over the 2-hour arc. Without the refinement with GPS measurements, the geocenter position uncertainty would be greater than 10 cm, and the TOPEX altitude determination error would be greater than 14 cm.

### VII. Summary and Conclusions

A geocentric coordinate frame provides a practical global reference system with a physically meaningful and unambigu-

ous definition of the coordinate origin. Two basic strategies for establishing a geocentric coordinate frame for GPS measurements have been investigated. All three cases of the first strategy make use of the precise relative positions which have been predetermined by VLBI to fix the frame orientation and the absolute scaling, while the offset from the geocenter is determined from GPS measurements. The reference frame thus adopted is consistent with the VLBI coordinate system. The second strategy establishes a reference frame by holding only the longitude of one of the tracking sites fixed. The absolute scaling is inferred by the adopted gravitational constant (GM) of Earth; the orientation in latitude is inferred from the time signature of Earth rotation in the GPS measurements. The coordinate system thus defined is a geocentric Earth-fixed coordinate system. The covariance analysis has shown that geocentric positioning to an accuracy of a few centimeters can be achieved with just a one-day arc of precise GPS pseudorange and carrier phase data.

Each of the two strategies has its advantages in different applications. The first strategy should be adopted in applications requiring a coordinate frame consistent with the VLBI reference frame. Among these applications are the monitoring of crustal motions in areas which have been investigated by VLBI observations and the determination of the Earth rotation parameters, viz., polar motion and variation of UT1-UTC. The second strategy, which holds the longitude at a reference site fixed, strictly limits itself in an ECEF frame established by the adopted values for the fixed longitude and the GM of Earth, and by GPS measurements. This method provides a superior result as long as the precise applications are within the same ECEF frame. Applications in which such an ECEF coordinate frame can be adopted include datum definition and network densification in an area where ECEF coordinates are appropriate. Various topographic and oceanographic surveys and prospecting surveys can benefit from its simplicity. In TOPEX orbit determination, this method can also be very convenient if a CTS frame such as WGS 84 is adopted.

#### References

- B. W. Parkinson and S. W. Gilbert, "NAVSTAR: Global Positioning System-Ten Years Later," Proc. IEEE, vol 71, no. 10, pp. 1177-1186, Oct. 1983.
- [2] R. J. Milliken and C. J. Zoller, "Principles of Operation of NAVSTAR and System Characteristics," *Navigation*, vol. 2, no. 2, pp. 95-106, Summer 1978.
- [3] T. P. Yunck, W. G. Melbourne, and C. L. Thornton, "GPS-Based Satellite Tracking System for Precise Positioning," *IEEE Trans. Geosci. & Remote Sensing*, vol. GE-23, no. 4, Jul. 1985.
- [4] T. P. Yunck, S. C. Wu, and J. T. Wu, "Strategies for Sub-Decimeter Satellite Tracking with GPS," *Proc.* 1986 IEEE Position Location and Navigation Symp., Las Vegas, NV, Nov. 1986.
- [5] Department of Defense World Geodetic System 1984, DMA Tech. Rep. 8350.2, The Defense Mapping Agency, Sep. 1987.
- [6] E. R. Swift, "NSWC's GPS Orbit/Clock Determination System," *Proc. First Int. Symp. on Precise Positioning with GPS*, Rockville, MD, pp. 51-62, Apr. 1985.
- [7] J. M. Davidson, et al., "The March 1985 Demonstration of the Fiducial Concept for GPS Geodesy: A Preliminary Report," *Proc. First Int. Symp. on Precise Positioning with GPS*, Rockville, MD, pp. 603-611, Apr. 1985.
- [8] O. J. Sovers, et al., "Radio Interferometric Determination of Intercontinental Baselines and Earth Orientation Utilizing Deep Space Network Antennas: 1971 to 1980," J. Geophys. Res., vol. 89, no. B9, pp. 7597-7607, Sep. 1984.
- [9] S. M. Lichten and J. S. Border, "Strategies for High-Precision Global Positioning System Orbit Determination," J. Geophys. Res., vol. 92, no. B12, pp. 12751– 12762, Nov. 1987.
- [10] G. H. Born, R. H. Stewart, and C. A. Yamarone, "TOPEX-A Spaceborne Ocean Observing System," in *Monitoring Earth's Ocean, Land, and Atmosphere from Space-Sensors, Systems, and Applications*, A. Schnapf (ed.), AIAA, Inc., New York, NY, pp. 464-479, 1985.
- [11] J. M. Dow and L. G. Agrotis, "Earth Rotation, Station Coordinates and Orbit Solutions from Lageos during the MERIT Campaign," Proc. Int. Conf. on Earth Rotation and Terrestrial Reference Frame, Columbus, OH, pp. 217-235, Jul. 1985.
- [12] G. H. Kaplan, "The IAU Resolutions of Astronomical Constants, Time Scales, and the Fundamental Reference Frame," USNO Circular, no. 163, U. S. Naval Observatory, Washington, DC, Dec. 1981.
- [13] I. I. Mueller, Spherical and Practical Astronomy as Applied to Geodesy, F. Ungar Publishing Co., Inc., 1969.
- [14] W. G. Melbourne, et al., MERIT Standards, IAU/IUGG Joint Working Group on Rotation of Earth, Project MERIT, 1983.
- [15] S. C. Wu and C. L. Thornton, "OASIS—A New GPS Covariance and Simulation Analysis Software System," *Proc. First Int. Symp. on Precise Positioning with GPS*, Rockville, MD, pp. 337–346, Apr. 1985.
- [16] S. C. Wu, T. P. Yunck, and C. L. Thornton, "Reduced-Dynamic Technique for Precise Orbit Determination of Low Earth Satellites," AAS paper 87-410, AAS/ AIAA Astrodynamics Specialists Conf., Kalispell, MT, Aug. 1987.

Table 1. Error sources and other assumptions for Strategy 1 (fixing baselines)

Reference site:	Goldstone
Other fiducial sites:	Canberra, Madrid
Nonfiducial sites:	Brazil, Japan, South Africa
GPS constellation:	18 satellites in 6 orbital planes
Cutoff elevation:	10 degrees
Data type:	P-code pseudorange; carrier phase
Data span:	6-34 hours
Data interval:	30 minutes
Data noise:	5 cm-pseudorange; 0.5 cm-carrier phase
Carrier phase bias:	10 km (adjusted)
Clock bias:	3 μsec-white noise (adjusted)
GPS epoch state:	10 m; 1 mm/sec (adjusted)
Geocenter position:	10 m each component (adjusted)
Baseline coordinates:	3 cm each component-fiducial; 10 cm each component-nonfiducial (adjusted)
Zenith troposphere:	Random walk parameter (adjusted): 20 cm bias; 1.3 cm batch to batch
Earth's GM:	One part in 108
Solar pressure:	10%
(UT1-UTC) rate:	10 m/day (adjusted)
Polar motion $(x_p, y_p)$ :	10 m (adjusted)

Table 2. Variations of assumptions from Table 1 for Strategy 2 (fixing only one longitude)

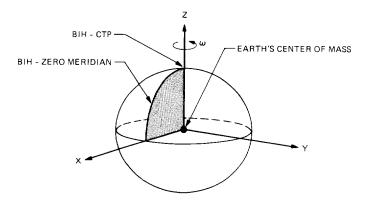
Reference site:	Goldstone
teference site coordinates: (adjusted)	10 m (latitude) 0 m (longitude) 10 m (height)
Other site coordinates: (adjusted)	10 m each component

Table 3. Fiducial baselines in Strategy 1

Case	Baselines	Adjusted	a priori
A	Goldstone-Canberra	no	3 cm
	Goldstone-Madrid	no	3 cm
В	Goldstone-Canberra	yes	3 cm
	Goldstone-Madrid	yes	3 cm
C Goldstone-Canberra Goldstone-Madrid	Goldstone-Canberra	yes	10 cm
	Goldstone-Madrid	no	3 cm

Table 4. Variations of assumptions from Table 1 for TOPEX orbit determination

Data span:	2 hours
Data interval:	5 minutes
TOPEX epoch state:	1 km; 1 m/sec (adjusted)
3-D force on TOPEX:	Process-noise (adjusted): $0.50 \mu m/s^2$ bias; $0.35 \mu m/s^2$ batch to batch
Gravity:	50% of current uncertainty (20 × 20 lumped)
Geocenter:	4 cm each component



ORIGIN: EARTH'S CENTER OF MASS

Z AXIS. PARALLEL TO DIRECTION OF THE CONVENTIONAL TERRESTRIAL POLE (CTP) FOR POLAR MOTION AS DEFINED BY THE BIH ON THE BASIS OF THE COORDINATES ADOPTED FOR THE BIH STATIONS

X AXIS: INTERSECTION OF THE ZERO MERIDIAN PLANE DEFINED BY BIH (WGS 84 REFERENCE MERIDIAN PLANE) AND THE PLANE OF CTP EQUATOR

Y AXIS: MEASURED IN THE PLANE OF CTP EQUATOR,  $\pi/2$  EAST OF X AXIS, THUS COMPLETING THE RIGHT-HANDED EARTH-CENTERED, EARTH-FIXED (ECEF) ORTHOGONAL COORDINATE SYSTEM

Fig. 1. The WGS 84 coordinate system.

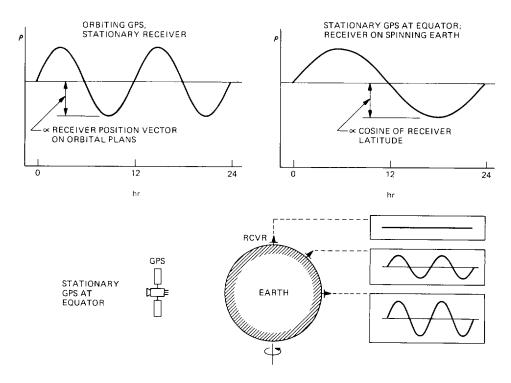


Fig. 2. Time signature of GPS measurements.

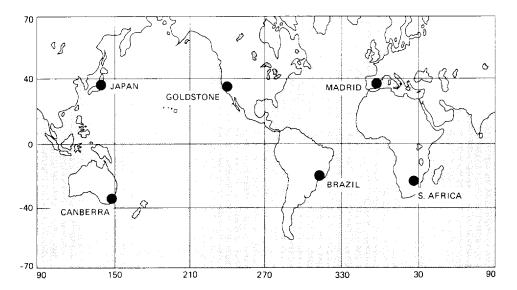


Fig. 3. A global GPS tracking network.

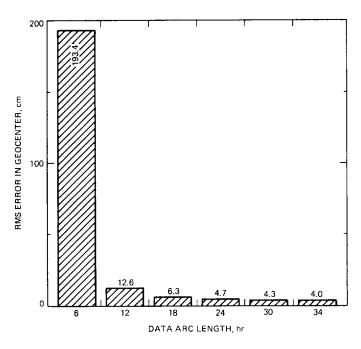


Fig. 4. Convergence of geocenter offset determination using Case A of Strategy 1 (two baselines fixed).

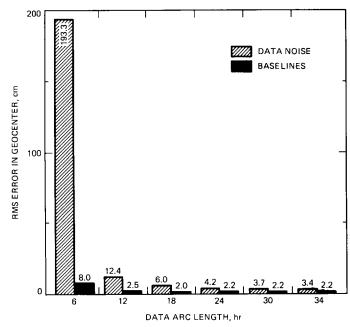
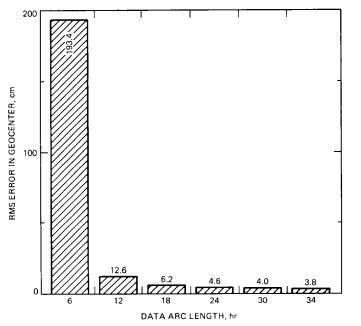


Fig. 5. Breakdown of geocenter offset determination error using Case A of Strategy 1 (two baselines fixed).



DATA NOISE
BASELINES

12.9

7.6

12.9

6.5

1.6

4.8

1.8

4.2

1.7

4.0

1.7

DATA NOISE
BASELINES

Fig. 6. Convergence of geocenter offset determination using Case B of Strategy 1 (two constrained baselines).

Fig. 8. Breakdown of geocenter offset determination error for Case C of Strategy 1 (one baseline fixed).

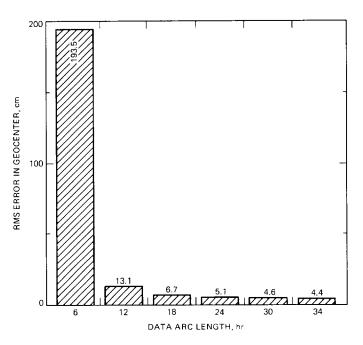


Fig. 7. Convergence of geocenter offset determination using Case C of Strategy 1 (one baseline fixed).

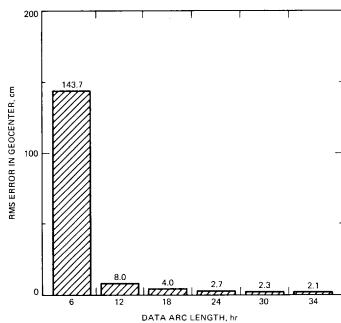


Fig. 9. Convergence of geocenter offset determination using Strategy 2 (longitude at Goldstone fixed).

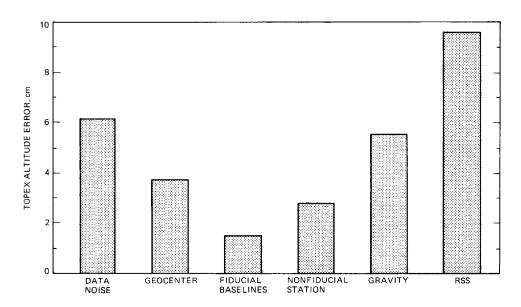


Fig. 10. Breakdown of TOPEX altitude determination error.

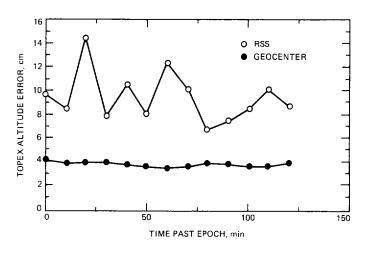


Fig. 11. Total TOPEX altitude error and effects of 4-cm geocenter error over a 2-hour period.

## **Appendix**

## Measurement Partial Derivatives with Respect to Baseline Components

Let the cartesian coordinates of the set of N tracking sites be  $(x_1, y_1, z_1), (x_2, y_2, z_2), \ldots, (x_N, y_N, z_N)$ . We can form the following baseline components:

$$b_{x,j} = x_j - x_1,$$
  $x \to y, z;$  (A-1)

where site 1 has been selected as the reference site with which all baselines are formed. For completeness, we also define

$$b_{x,1} = x_1, \qquad x \to y, z \tag{A-2}$$

for the reference site. For simplicity, but without loss of generality, partial derivatives with respect to only the x-component of baselines will be derived. The relation for the other two components follows directly. These equations can be rearranged as

$$x_{j} = \begin{cases} b_{j}, & j = 1 \\ b_{i} + b_{1}, & j = 2, 3, \dots, N \end{cases}$$
 (A-3)

from which the following partial derivative can be formed:

$$\frac{\partial \mathbf{x}_{i}}{\partial b_{x,j}} = \begin{cases} 1, & j = 1 \\ \delta_{ij}, & j = 2, 3, \dots, N \end{cases}$$
 (A-4)

where  $\delta_{ij}$  is the Kronecker delta. The partial derivative of a measurement R with respect to the baseline components  $b_j$  can be expressed in terms of those with respect to the site coordinates  $x_j$  by the following chain rule:

$$\frac{\partial R}{\partial b_{x,j}} = \frac{\partial R}{\partial x_1} \frac{\partial x_1}{\partial b_{x,j}} + \frac{\partial R}{\partial x_2} \frac{\partial x_2}{\partial b_{x,j}} + \dots + \frac{\partial R}{\partial x_N} \frac{\partial x_N}{\partial b_{x,j}}$$
(A-5)

which, with the substitution of Eq. (A-4), becomes

$$\frac{\partial R}{\partial b_{x,j}} = \begin{cases} \sum_{n=1}^{N} \frac{\partial R}{\partial x_n}, & j = 1\\ \frac{\partial R}{\partial x_j}, & j = 2, 3, \dots, N \end{cases}$$
(A-6)

Hence, the partial derivative of the measurement with respect to a cartesian component of a baseline is the same as that with respect to the same component of the nonreference site forming the baseline; and the partial derivative with respect to a component of the reference site is the sum of all partial derivatives with respect to the same component of all sites forming the baselines.